## 8.2 The Type 3: An Origin Pole plus a Double Pole/Zero Pair

The type 3 compensator offers a larger phase boost than its type 2 counterpart. Unfortunately, because of the fixed internal 7-kHz pole present in the duty ratio modulator and the limit set for the resistor  $R_s$ , we cannot expect the full flexibility as with a traditional op amp approach. That being said, let us have a look at a type 3 implementation as it appears in Figure 8.10. The principle remains the same: how do we add another pole/zero pair given the fast lane presence? As we did for the TL431 with a voltage-mode feedback control, a RC network will be added in parallel with the LED series resistor. The network will add the zero/pole pair we are looking for in a type 3 architecture. As we already derived the transfer function of the type 2-see (8.8)—going to the type 3 simply requires us to replace  $R_{LED}$  with the equivalent impedance brought by the new network  $Z_{LED}$  highlighted in Figure 8.10:

$$Z_{LED} = \frac{R_{LED} \left( R_3 + \frac{1}{sC_3} \right)}{R_{LED} + \left( R_3 + \frac{1}{sC_3} \right)} = R_{LED} \frac{sR_3C_3 + 1}{sC_3 \left( R_{LED} + R_3 \right) + 1}$$
(8.32)

Now substituting this expression in (8.8), we have

$$\frac{I_{FB}(s)}{V_{out}(s)} = \frac{CTR}{R_{LED}} \frac{1 + 1/sR_1C_1}{1 + sC_{V_{cc}}(R_s + R_d)} (1 + sR_sC_{V_{cc}}) \frac{sC_3(R_{LED} + R_3) + 1}{sR_3C_3 + 1}$$
(8.33)

The current  $I_{FB}(s)$  is injected into the duty ratio modulator whose transfer function includes a gain as described by (8.3), followed by a 7-kHz pole:



Figure 8.10 A type 3 implementation with a shunt regulator suffers from the limits imposed on R and the internal 7-kHz pole.

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